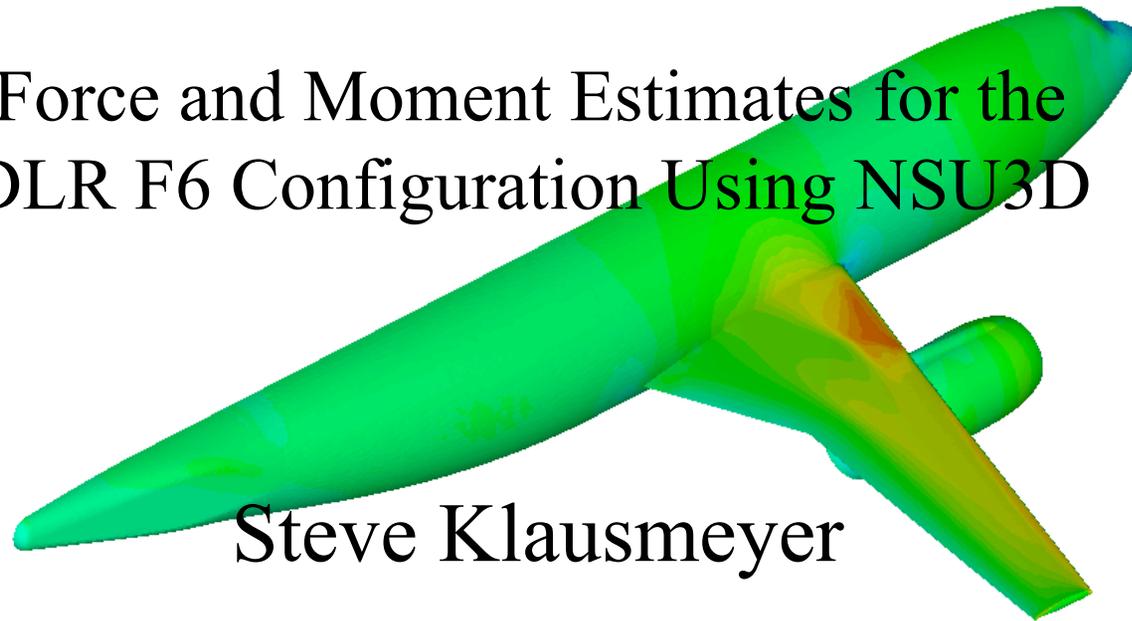




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Force and Moment Estimates for the DLR F6 Configuration Using NSU3D



Steve Klausmeyer

Cessna Aircraft Company



Goals

- Further refine and quantify in-house drag prediction
 - Evaluate incremental drag capability
- Evaluate ICEM for unstructured viscous mesh generation
 - Flow solver compatibility
 - Force and moment accuracy



NSU3D

- Unstructured grid, mixed element, node based
- Thin-layer RANS with Spalart-Allmaras turbulence model
- Multigrid with automated coarse level generation via agglomeration
- Implicit lines through boundary layer speed convergence
- Distributed memory parallel implementation
- Cache-based optimizations



ICEM

- Features
 - CATIA interface
 - Mesh sizes specified directly on patches
 - Multi-Use --> structured, unstructured, mixed
- Issues
 - Memory requirements for large meshes
 - Prism grid quality and robustness
 - Octree mesh growth



Mixed Element Unstructured Meshes



- Self-generated using the Tetra & Prism modules within ICEM
- 25 prism layers
- Isotropic surface elements

- WB grid sizes: 1.2m 2.6m 6.2m
- WBNP grid sizes: 1.6m 4.0m 8.0m

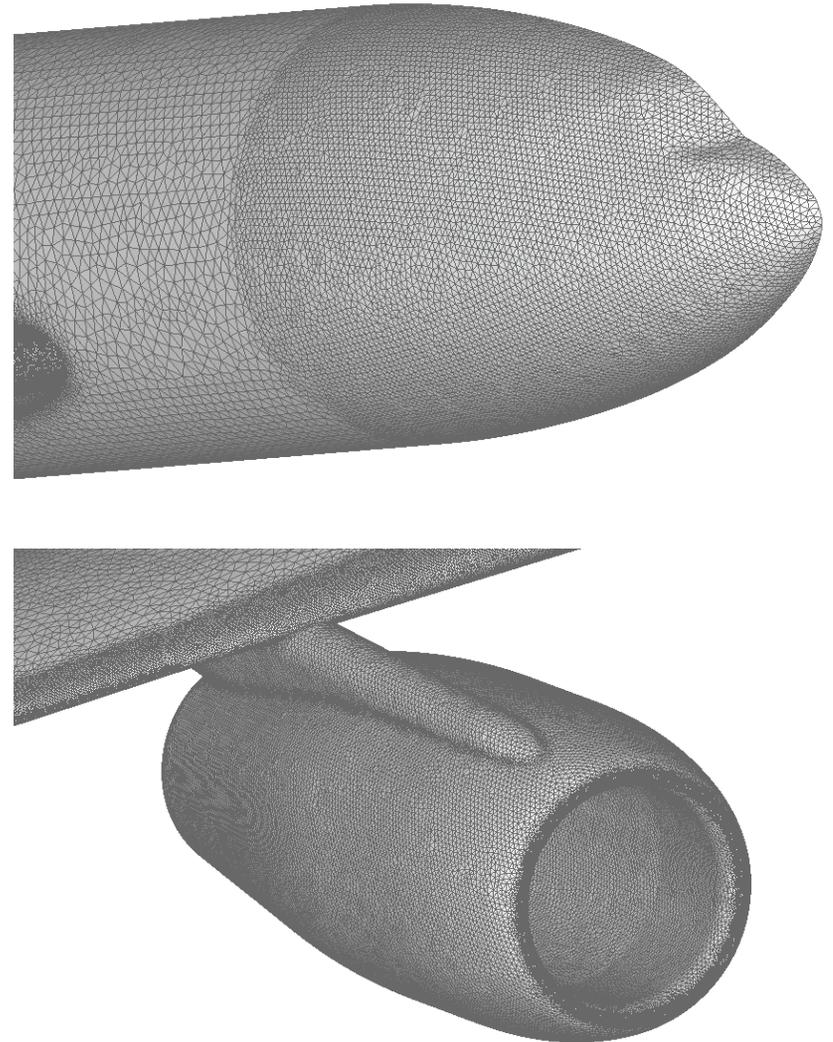
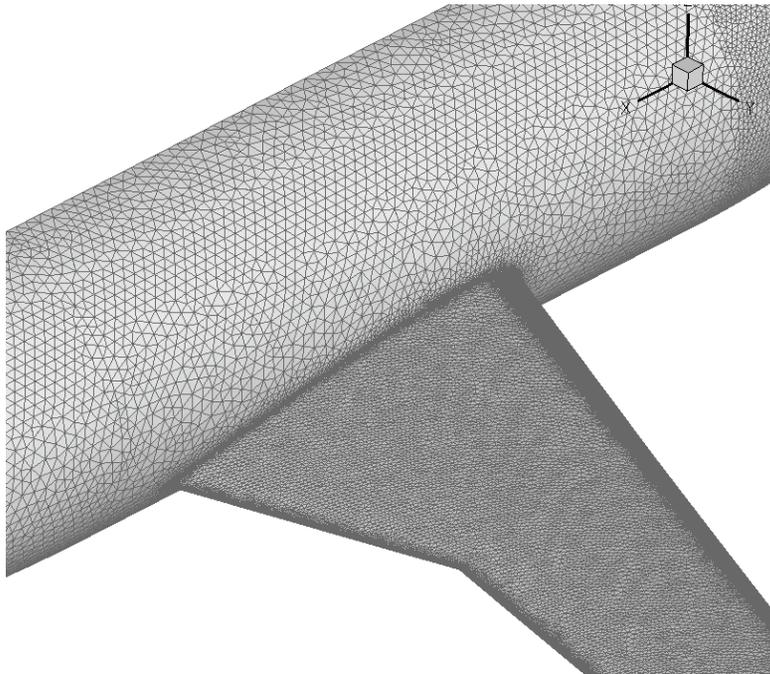
- Generation times: ~ 8 hours for medium WB mesh



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Surface Meshes - Medium





Computer Resources

- 48 node Linux cluster.
 - 1.7 GHz Athlon processors
 - 48 Gbyte total memory
 - 3 16 node banks
- 32 node Linux cluster
 - Alpha VP2000 motherboards
 - 32 Gbyte total memory
- 8 node SGI ONYX
 - 600 MHz R14000 processors
 - 6 Gbyte memory with 6 Gb swap



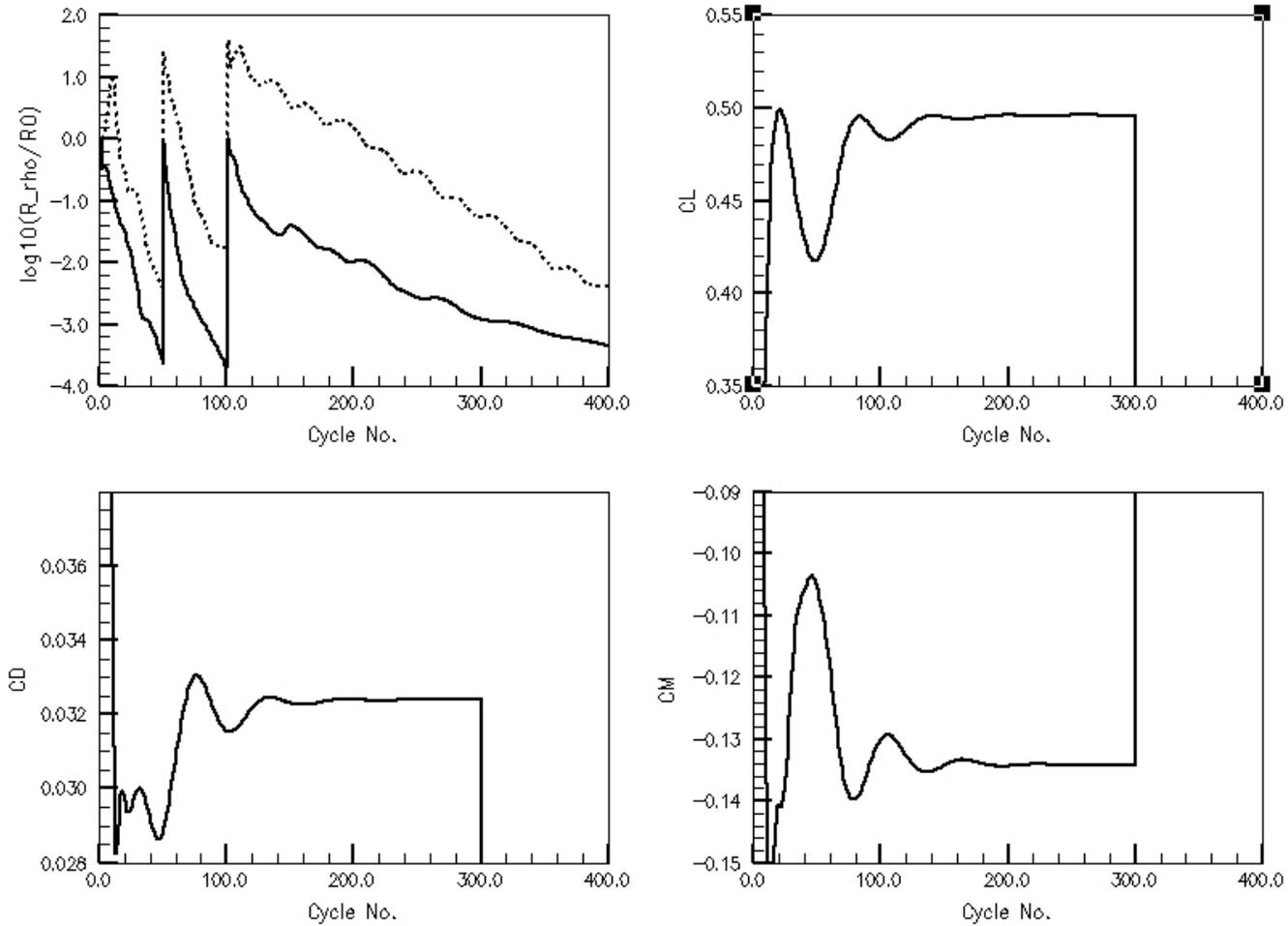
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Solution Statistics

- Each solution utilized 16 nodes
- For the medium WB mesh
 - 275 Mbytes per node (4.4 Gbytes total)
 - 3.6 hrs for 500 multigrid cycles
 - Drag polar or drag rise within a 24 hour window.

Typical Solution Convergence





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Flow Features

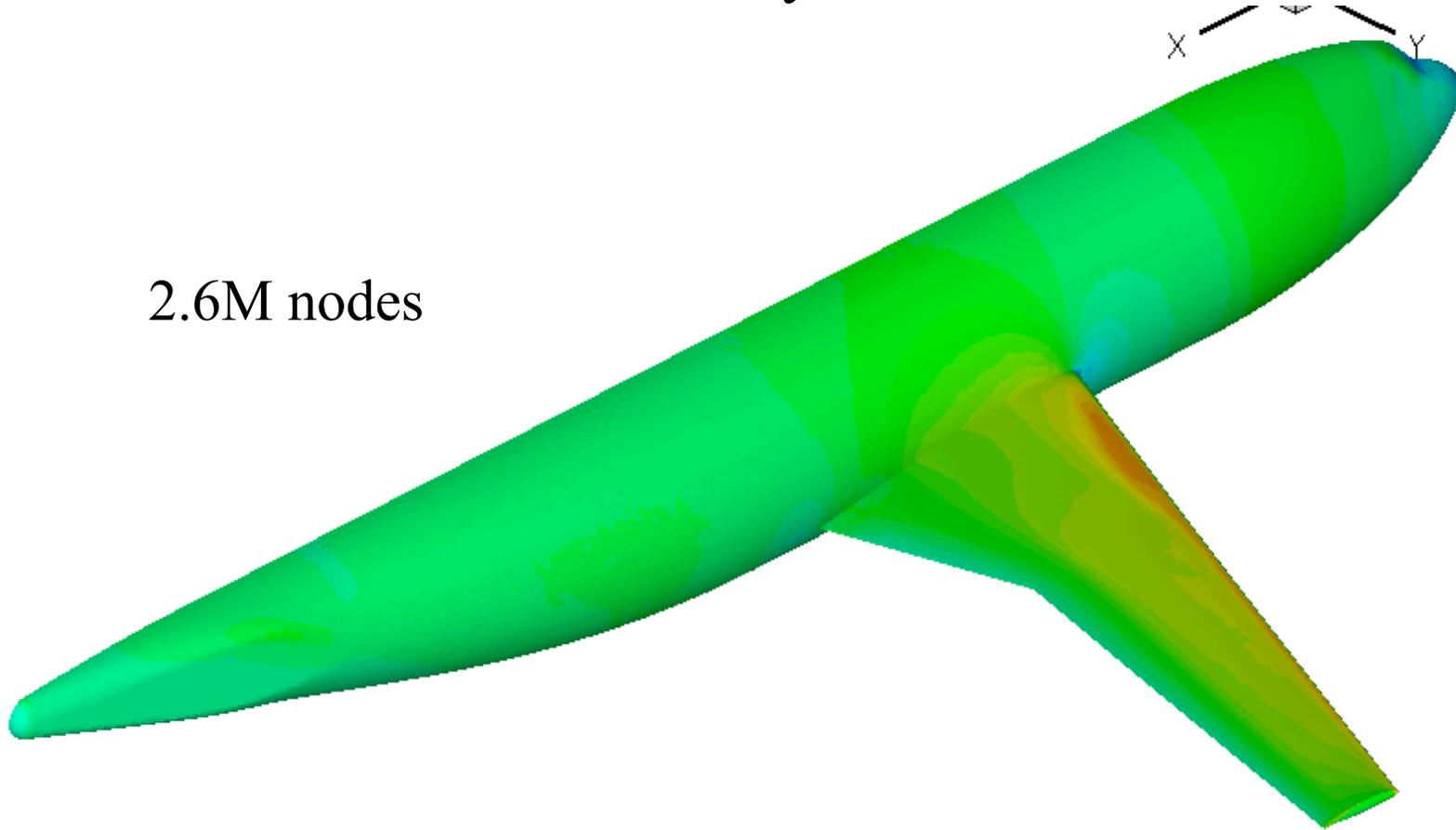


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WB Surface Pressure
 $M=0.75$ $CL=0.5$
 $Re=3M$ Fully Turbulent



2.6M nodes



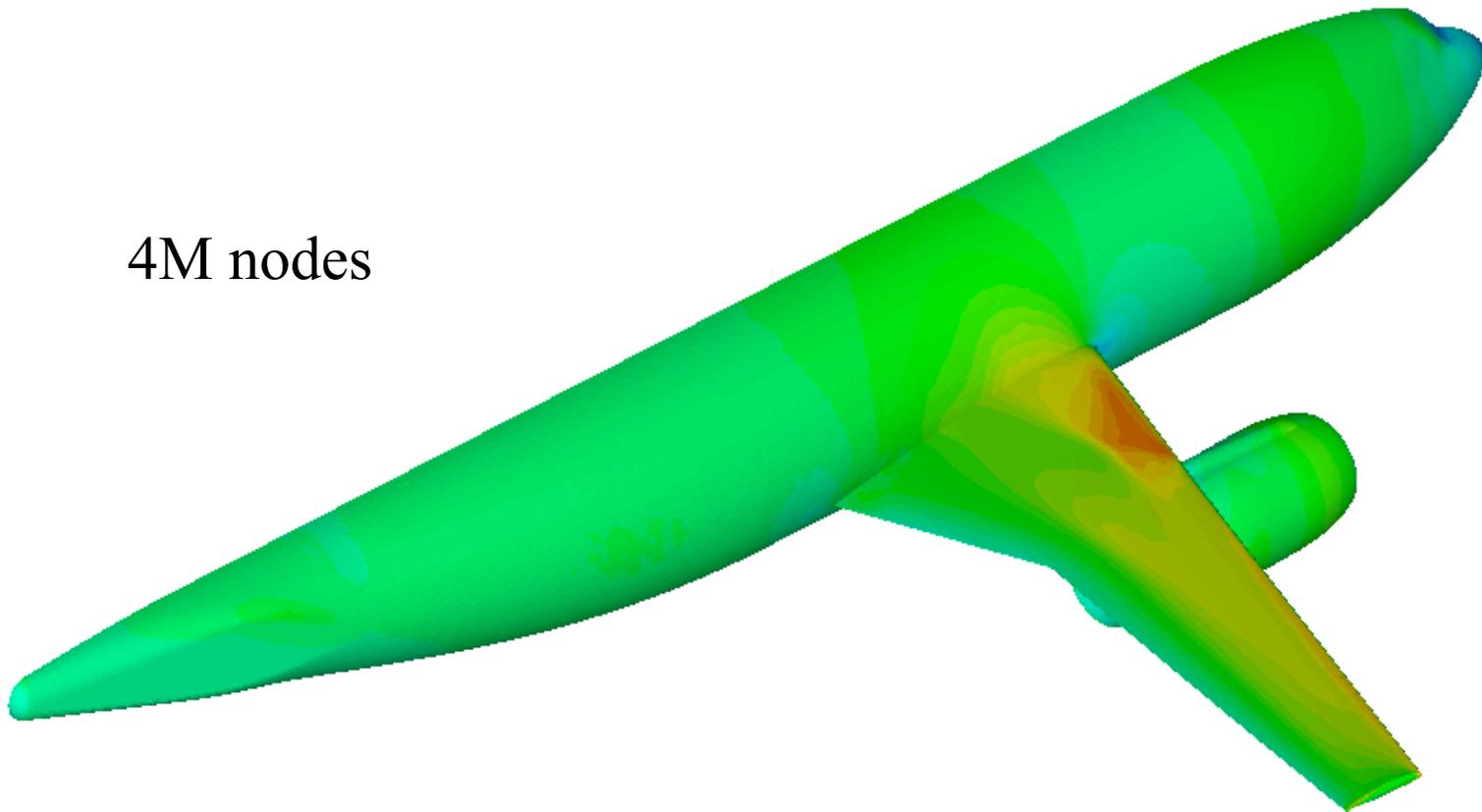


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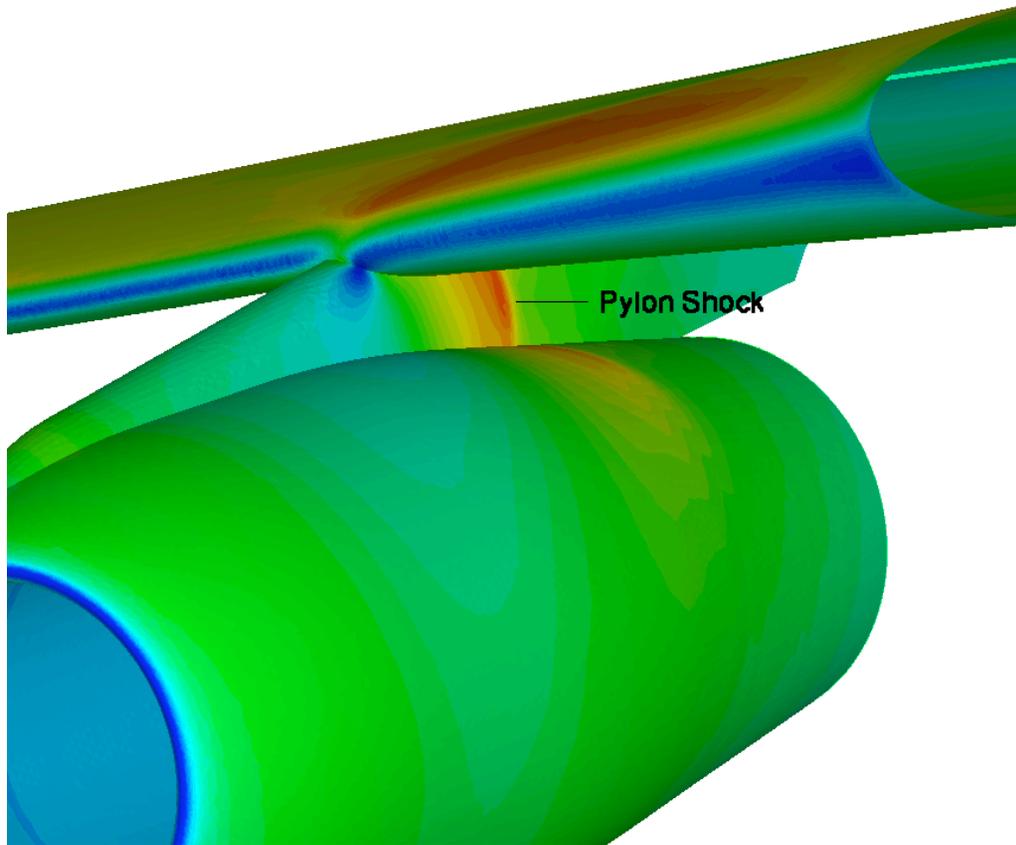


WBNP Surface Pressure
 $M=0.75$ $CL=0.5$
 $Re=3M$ Fully Turbulent

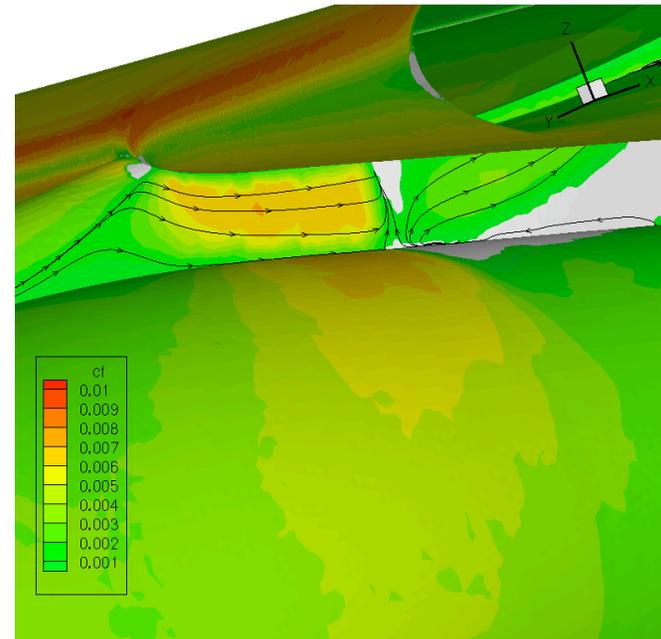
4M nodes



Flow Features

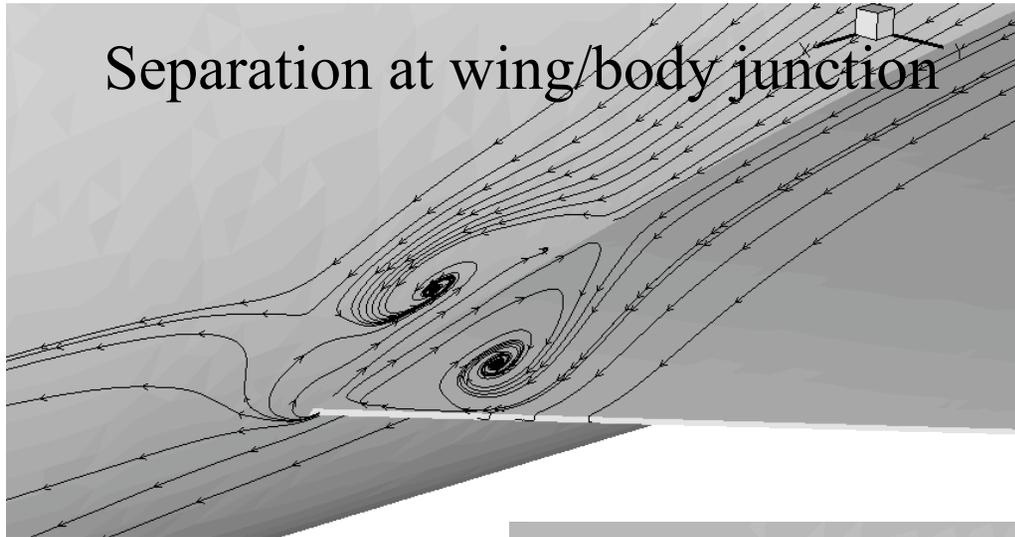


Pressure

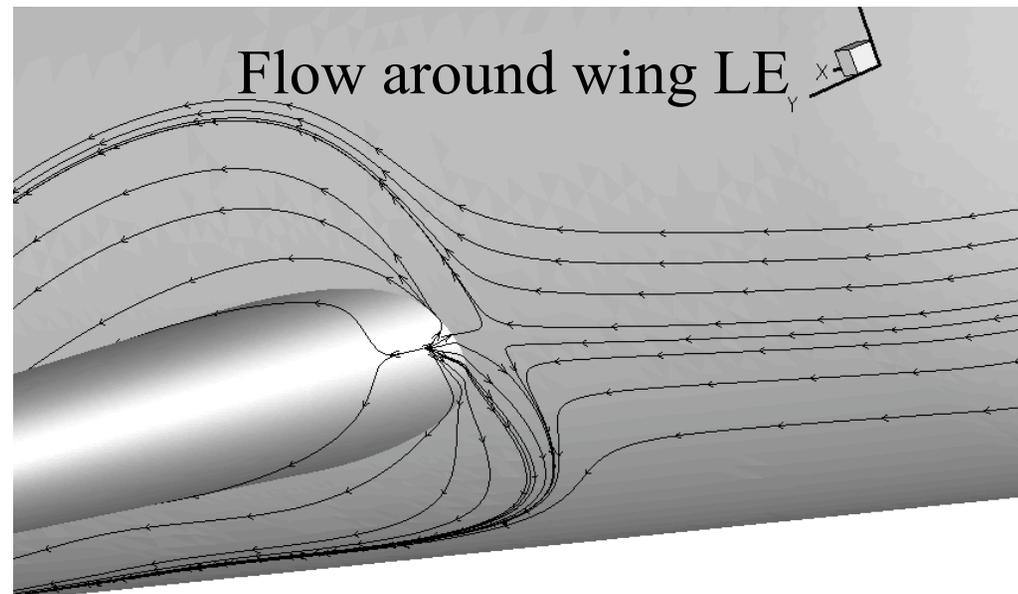
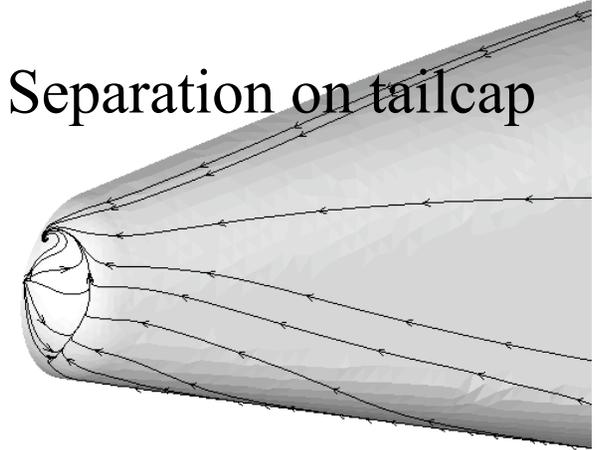


Skin Friction

Flow Features



Separation on tailcap



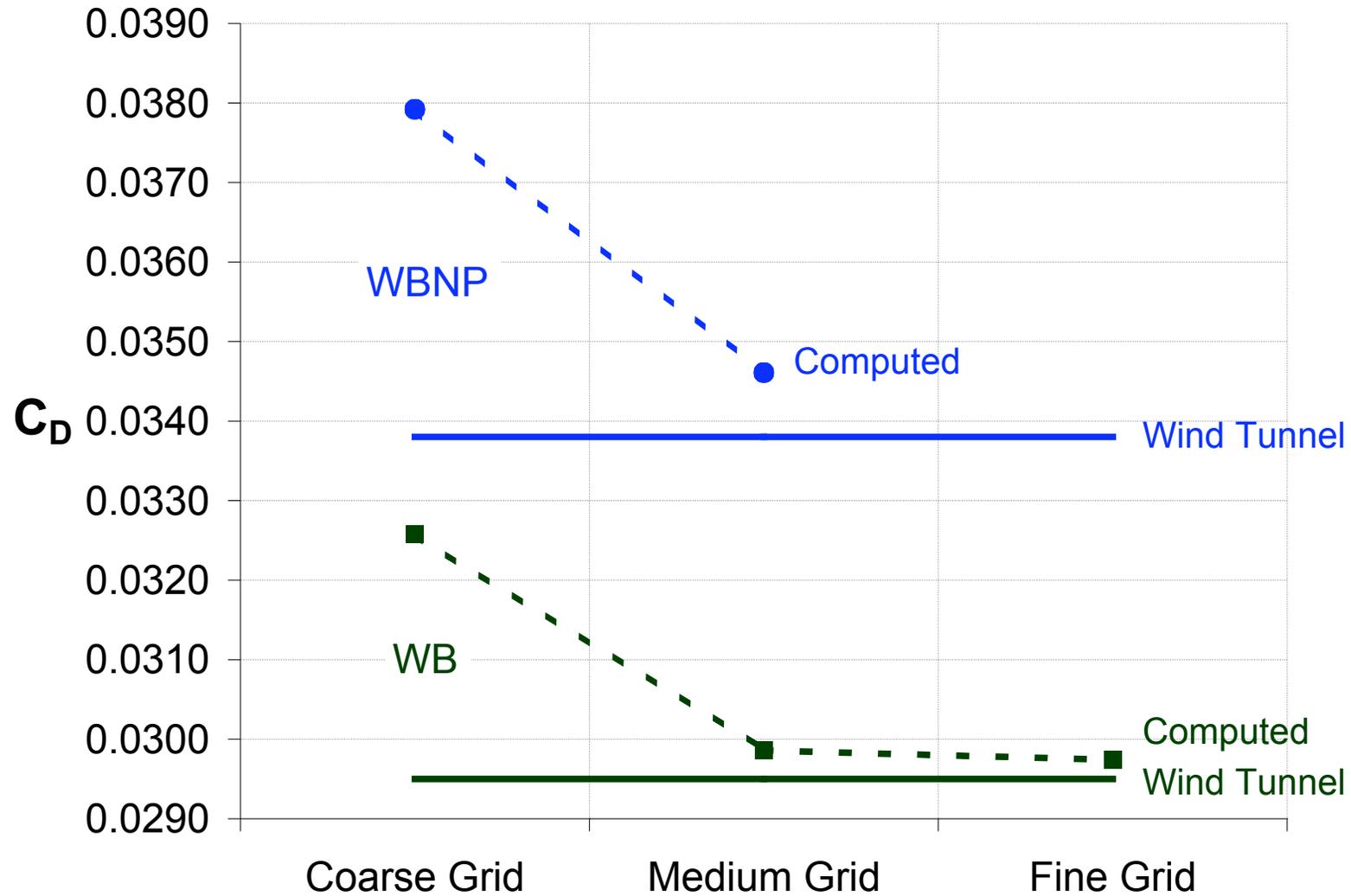


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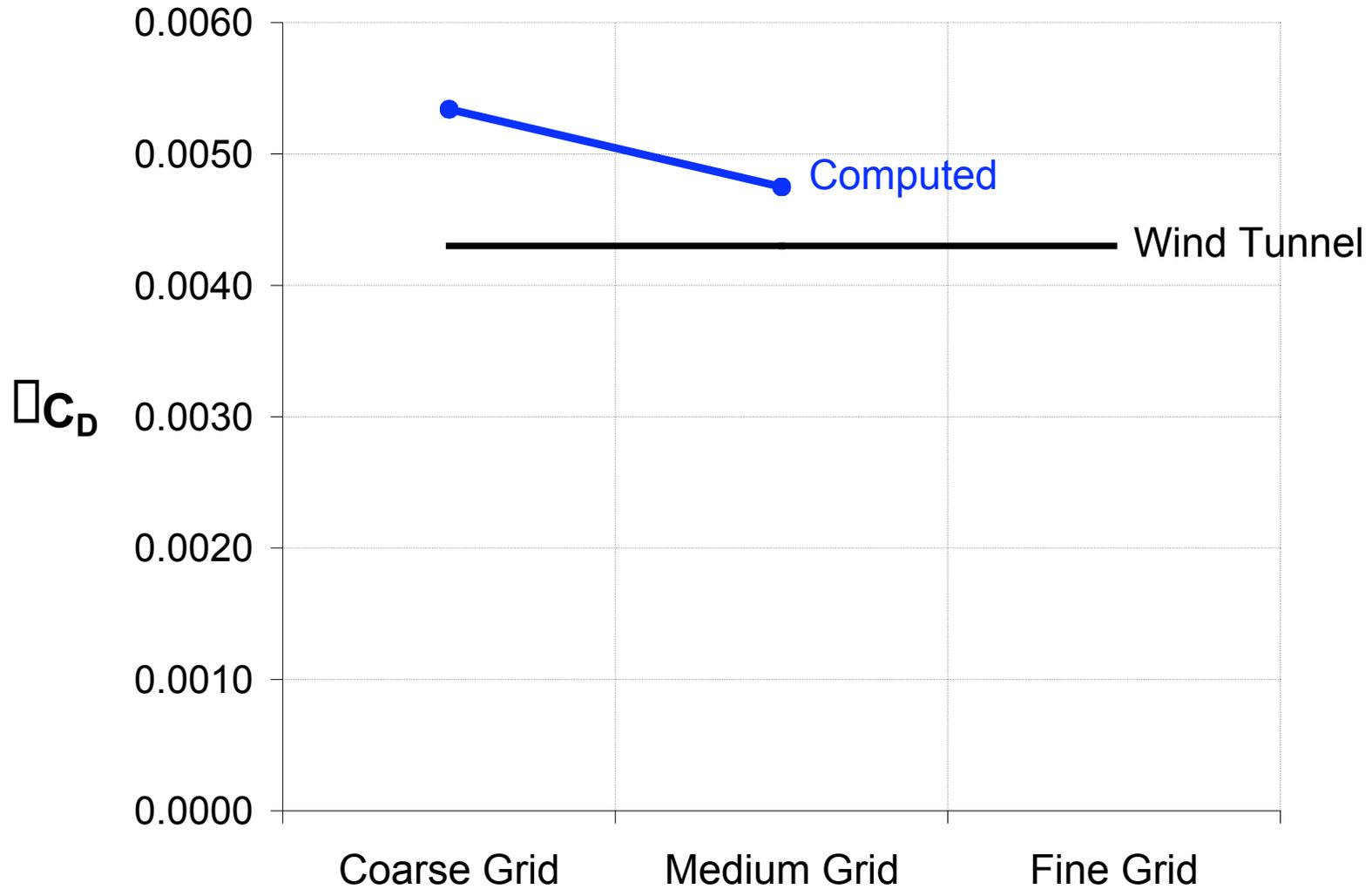
Case 1 – Grid Convergence

Effect of Grid Size on Drag

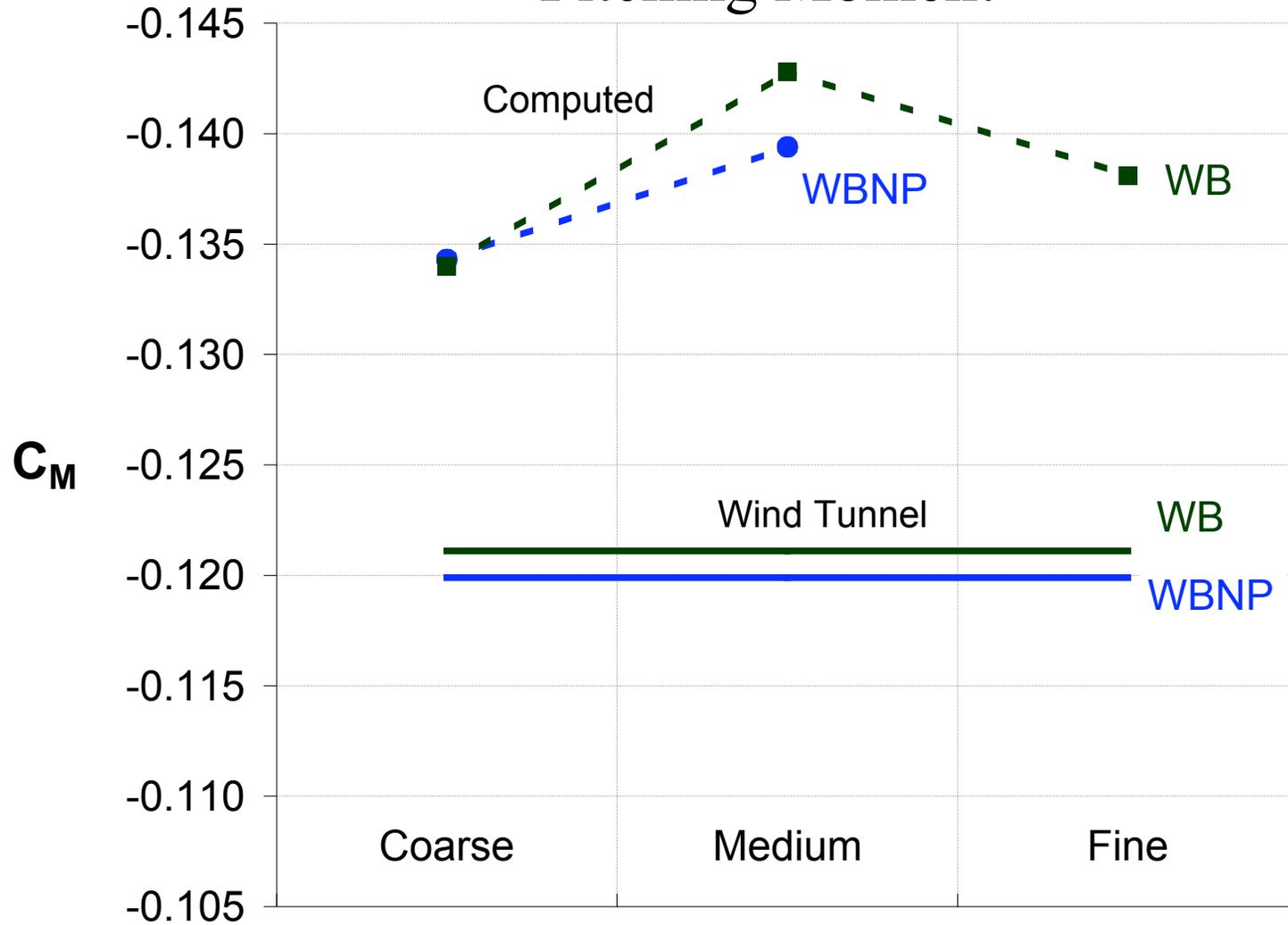




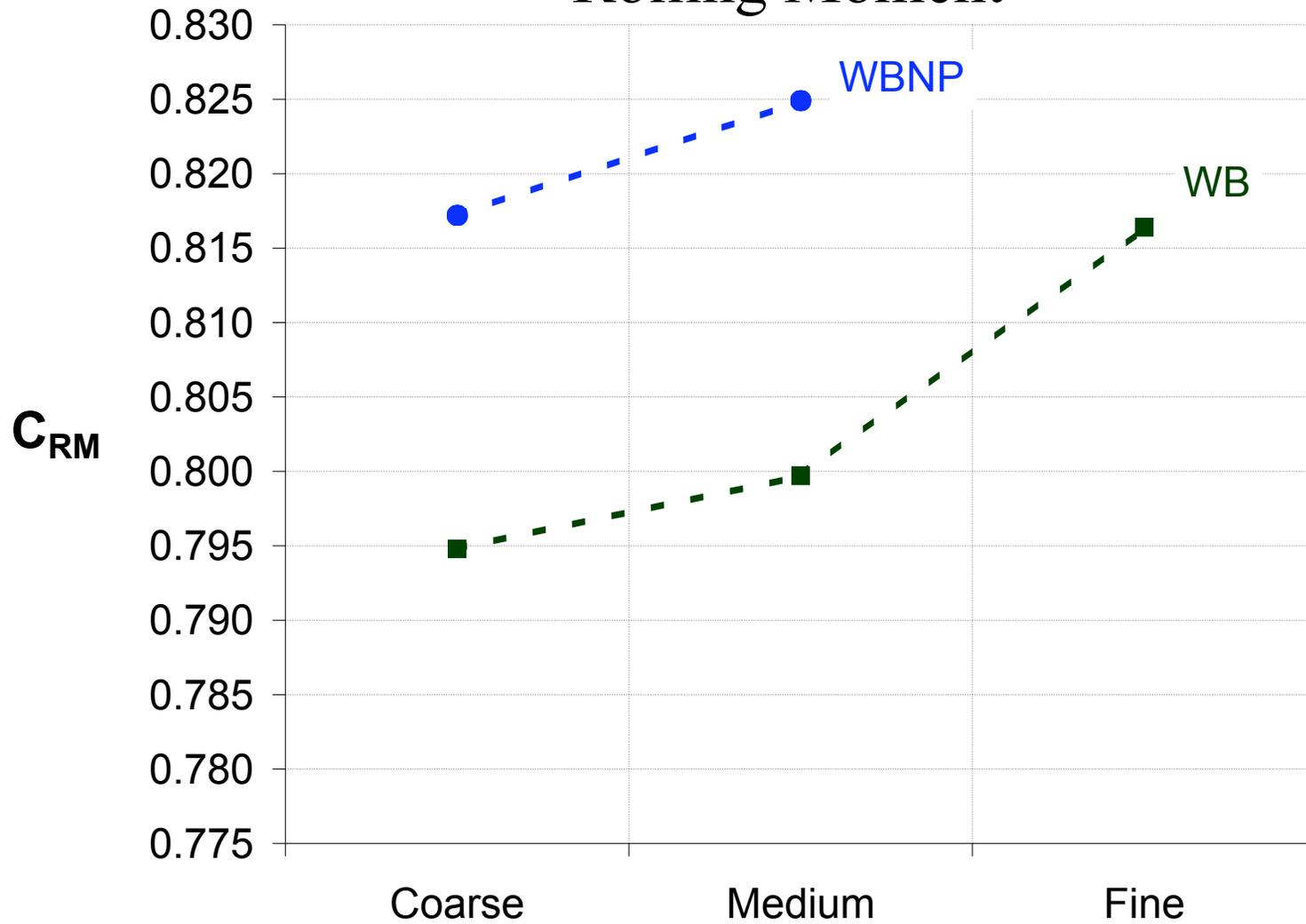
Effect of Grid Size on Nacelle Installation Drag



Effect of Grid Size on Pitching Moment

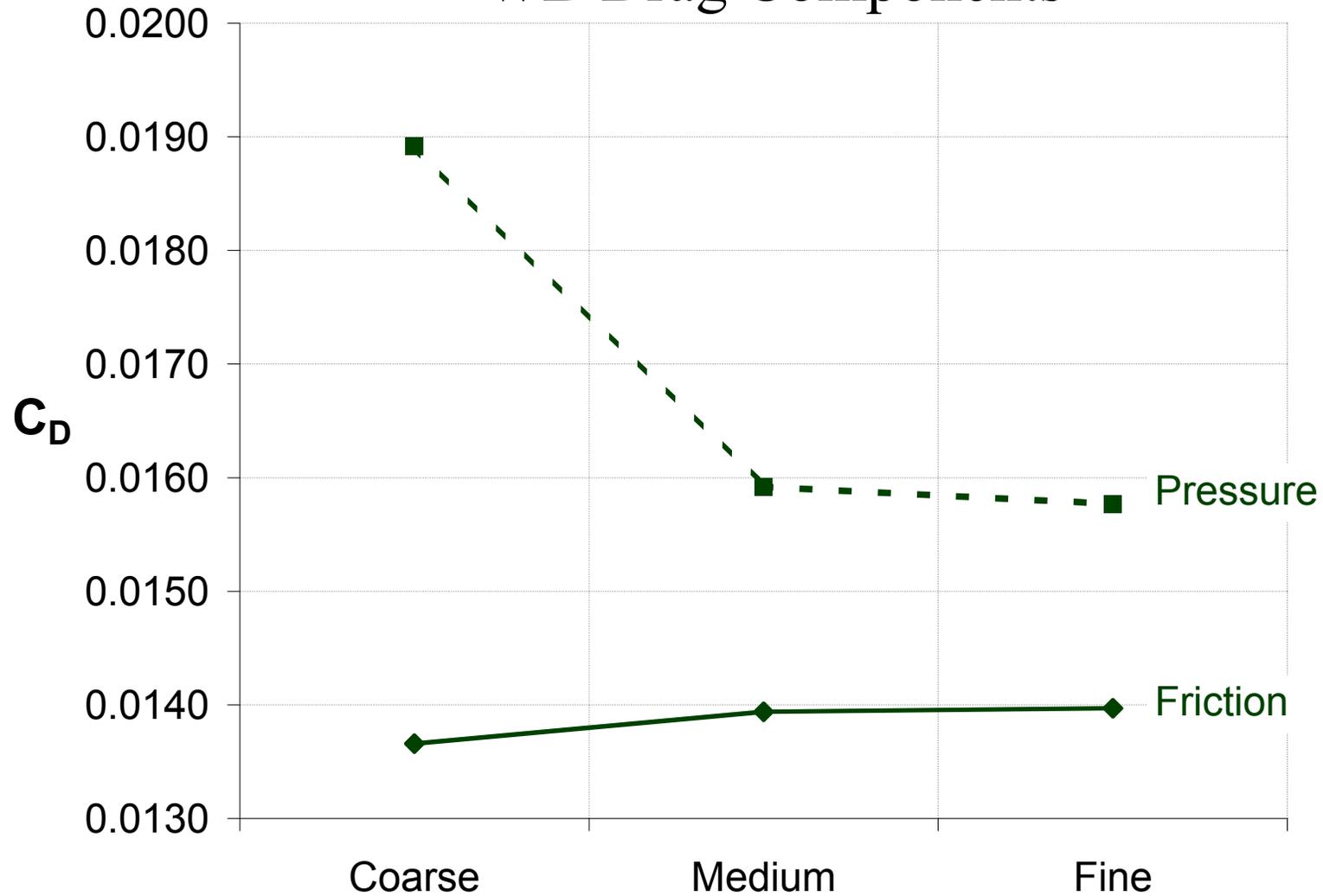


Effect of Grid Size on Rolling Moment



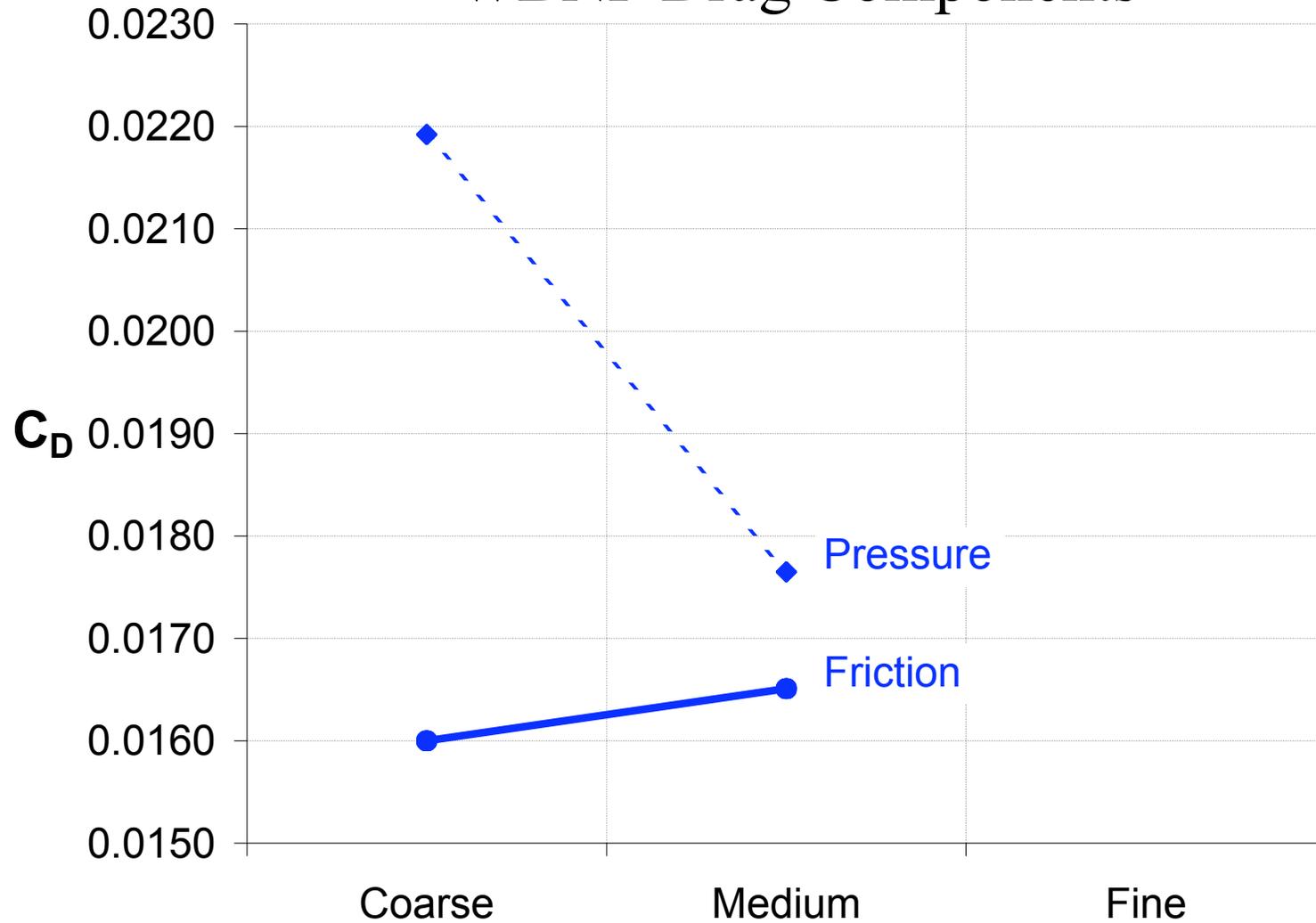


Effect of Grid Size on WB Drag Components





Effect of Grid Size on WBNP Drag Components



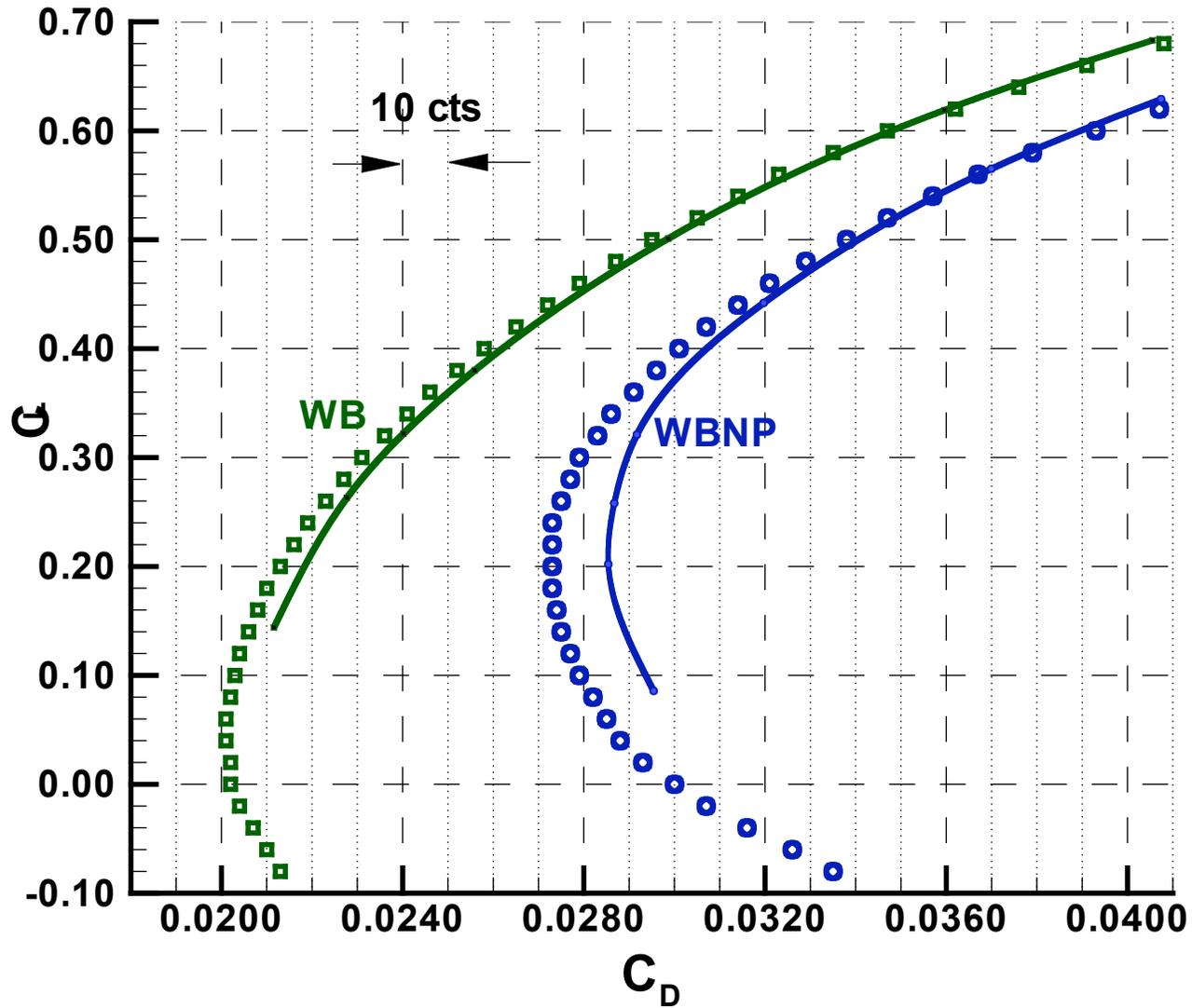


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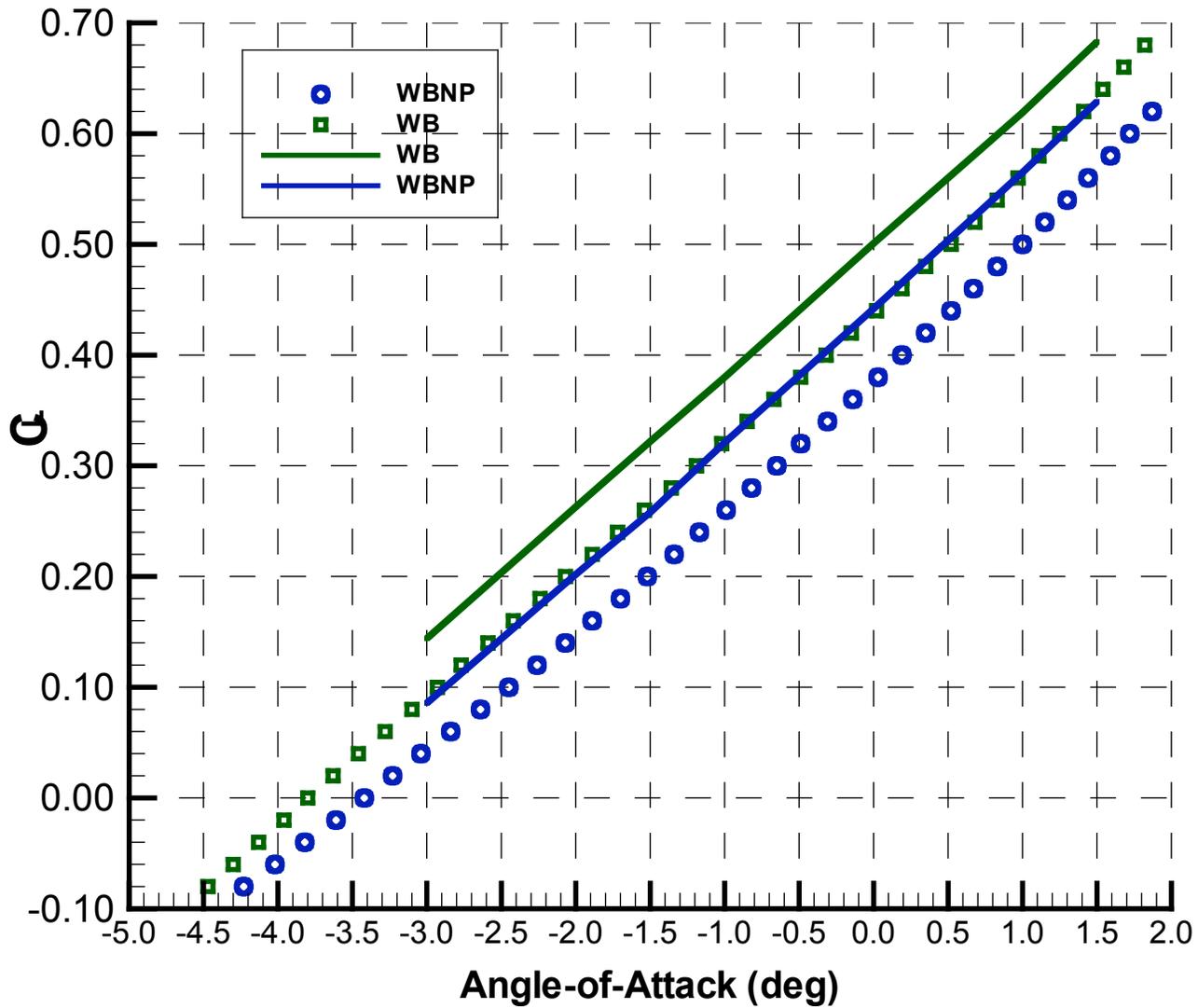


Case 2 – Alpha Sweep

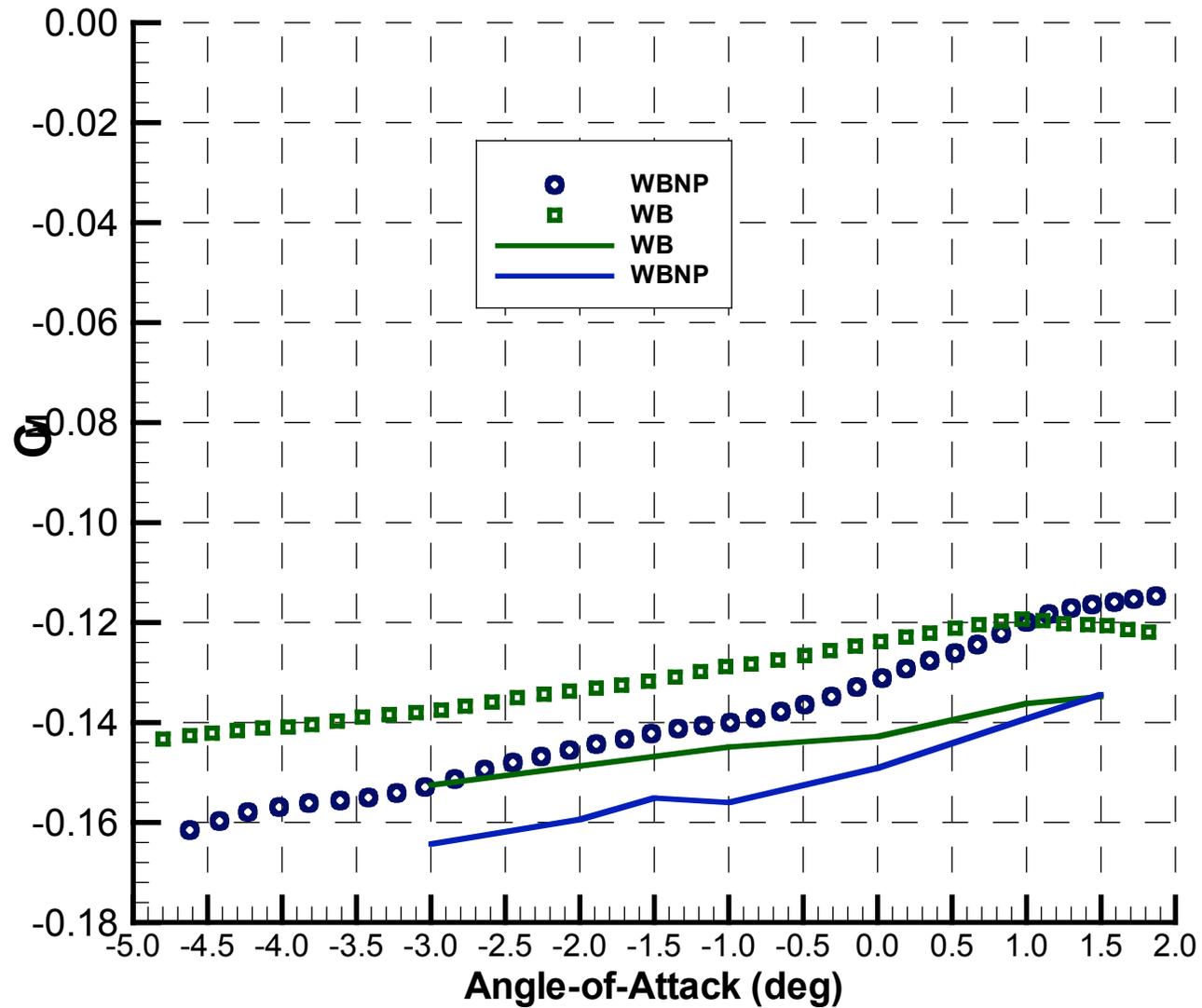
Drag Polar



Lift



Pitching Moment





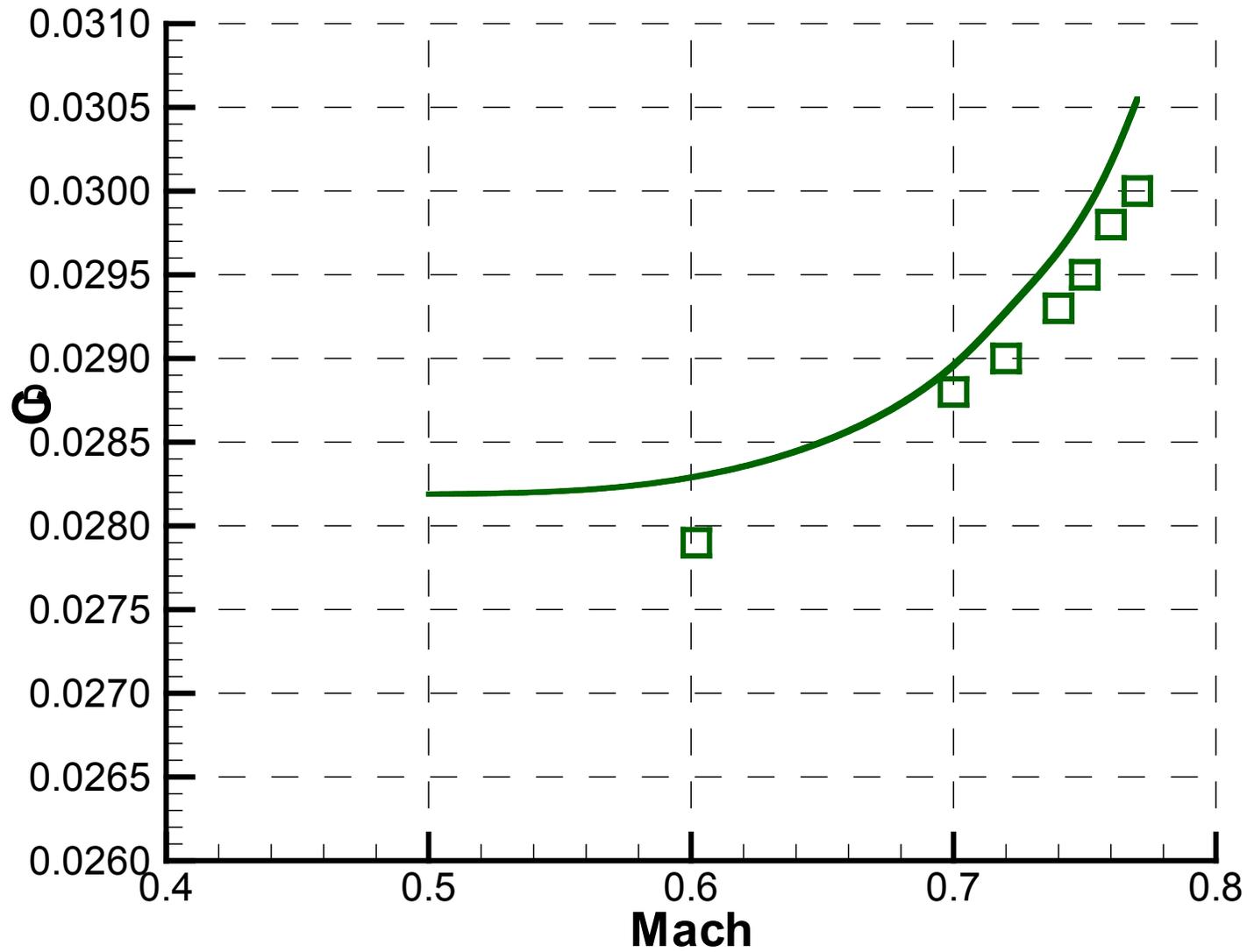
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Case 4 – Drag Rise

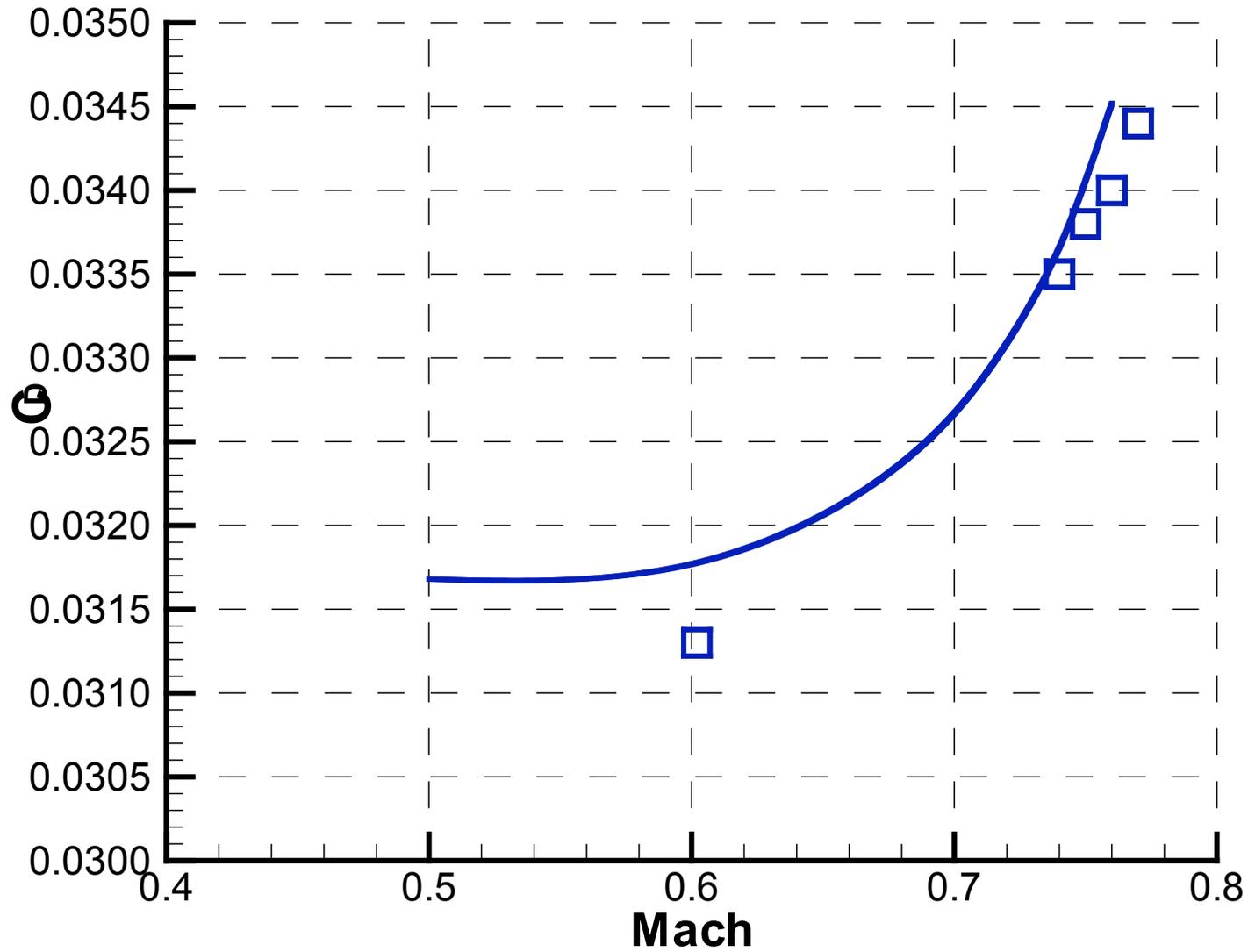


WB Drag Rise





WBNP Drag Rise





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Conclusions



This was a lot of work.



More Conclusions

- Current methodology approaching adequacy for prediction of drag changes due to minor airframe modifications.
- There is enough variation in parasite, induced, and wave drag characteristics to warrant further investigation before using to develop a full drag basis.
- Flow solver performance
 - Robust - tolerant of meshes with isolated regions of poor grid quality
 - No startup trauma difficulties
 - Fast convergence --> allows overnight drag polar runs
- Grid generation
 - Developed procedures for generating acceptable prism meshes.
 - Prism mesh robustness and quality is an issue.



Further Work

- Perform similar exercise on a business jet configuration with fuselage mounted nacelles.
- Tripped boundary layer study with new version of code.
- Study induced drag prediction at lower Mach number (0.5)
- Investigate alpha shift
 - Grid resolution
 - Comparisons with in-house configurations
- Investigate pitching moment discrepancy